





# Reflectance Models (BRDF)

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### Light travels through media



Absorption is simple, scattering is very complicated



### Light hits object surface (ideal)





#### Real surface (microscopic view)





#### Real surface (microscopic view)





#### What we see from the distance..



#### Metals (conductors)





#### **Dielectrics (insulators)**





#### **BSSRDF** idea





#### ("Bi-directional Scattering-Surface Reflectance Distribution Function")

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#### Ignoring exit-to-entry distance



#### **BRDF** = "Bi-directional Reflectance Distribution Function"

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#### Shading terms (components)



#### **BRDF** formulation





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### **BRDF** plausibility



energy-conserving
$$\int_{\Omega} f(\omega_i, \omega_o) (n \cdot \omega_i) d\omega_i \leq 1$$



- Beckmann, Spizzichino (1963): electromagnetic wave reflection on rough surfaces (optics)
- Torrance, Sparrow (1967): off-specular reflections on rough surfaces (optics)
- Phong (1975): famous empirical model, used many decades
- Blinn (1977): first light reflection presentation at SIGGRAPH
- Cook, Torrance (1981): generalization, implementation, first physically based BRDF model in computer graphics



- He (1991): more complex wave optics, polarization, diffraction, interference..
- **Ward** (1992): anisotropic material, microfacets
- Schlick (1994): fast Fresnel formula approximation, two-layer reflectance model
- **Lafortune** (1997): multiple lobes, fitted to lab data
- Ашихмин, Shirley (2000): anisotropic Phong
- Walter (2007): microfacet refraction model (BSDF = Bidirectional Scattering Distribution Function)
- Ашихмин, Bagher (2007, 2012): models based on arbitrary microfacet distribution (measured..)

#### BRDF ZOO I





#### BRDF ZOO II





#### Ideal diffusion





#### ideal diffuse material (Lambertian surface)

- reflection probability is constant
- examples: furry surface, noisy microstructure w/o any pattern

# Lambert law: reflected intensity depends solely on cos α

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# Ideal (mirror) reflection





 ratio of reflected and refracted light is determined by the Fresnel equations (19. century)

#### Refraction (Snell's law, Ibn Sahl, 984)



$$\cos\beta = \sqrt{1 - n_{12}^{2} \sin^{2} \alpha} = \sqrt{1 - n_{12}^{2} \cdot (1 - (n \cdot l)^{2})}$$
$$t = \left[ n_{12}(n \cdot l) - \sqrt{1 - n_{12}^{2} \cdot (1 - (n \cdot l)^{2})} \right] \cdot n - n_{12} \cdot l$$

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- going from more dense environment to less dense one (n<sub>1</sub> > n<sub>2</sub>)
- for incident angles greater than critical angle α<sub>tr</sub> there is no refraction at all!





- two **polarizations** (electric field perpendicular "s" /senkrecht/ or parallel "p" to the <u>incident plane</u>)
- reflectance "R" and transmittance "T" (power ratios):

$$R_{s} = \left[\frac{\sin(\beta - \alpha)}{\sin(\beta + \alpha)}\right]^{2} \qquad T_{s} = 1 - R_{s}$$
$$R_{p} = \left[\frac{\tan(\beta - \alpha)}{\tan(\beta + \alpha)}\right]^{2} \qquad T_{p} = 1 - R_{p}$$



#### Fresnel equations (alternative)

no need to compute angles (cosines are easy):

$$R_{s} = \left[\frac{n_{1}\cos\alpha - n_{2}\cos\beta}{n_{1}\cos\alpha + n_{2}\cos\beta}\right]^{2}$$
$$R_{p} = \left[\frac{n_{1}\cos\beta - n_{2}\cos\alpha}{n_{1}\cos\beta + n_{2}\cos\alpha}\right]^{2}$$

### **Unpolarized light**



• averaging values  $R_s a R_p$ :  $R = \frac{1}{2} \frac{(a-u)^2 + b^2}{(a+u)^2 + b^2} \left[ \frac{(a+u-1/u)^2 + b^2}{(a-u+1/u)^2 + b^2} + 1 \right]$  $a^{2} = \frac{1}{2} \left( \sqrt{(n_{\lambda}^{2} - k_{\lambda}^{2} + u^{2} - 1)^{2} + 4n_{\lambda}^{2}k_{\lambda}^{2}} + n_{\lambda}^{2} - k_{\lambda}^{2} + u^{2} - 1 \right)$  $b^{2} = \frac{1}{2} \left( \sqrt{(n_{\lambda}^{2} - k_{\lambda}^{2} + u^{2} - 1)^{2} + 4n_{\lambda}^{2}k_{\lambda}^{2}} - n_{\lambda}^{2} + k_{\lambda}^{2} - u^{2} + 1 \right)$  $u = \cos \alpha = n \cdot l$   $n = n_{\lambda} - i k_{\lambda}$  (for dielectric  $k_{\lambda} = 0$ )

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#### Dielectric (insulator) materials

• 
$$\mathbf{k}_{\lambda} = \mathbf{0} \implies$$

$$a^2 = n_\lambda^2 + u^2 - 1$$
  $b = 0$ 

$$R = \frac{1}{2} \frac{(a-u)^2}{(a+u)^2} \left( \frac{[u(a+u)-1]^2}{[u(a-u)+1]^2} + 1 \right)$$

#### Remarks (Fresnel)



- if  $\alpha = \pi/2$  (i.e.  $\mathbf{u} = \mathbf{0}$ ), then reflectance  $\mathbf{R}_{\lambda}(\mathbf{90}) = \mathbf{1}$ regardless of the wavelength  $\lambda$
- for perpendicular ray ( $\alpha = \mathbf{0}$ ):

$$R_{0} = R_{s} = R_{p} = \left(\frac{n_{2} - n_{1}}{n_{2} + n_{1}}\right)^{2}$$
$$T_{0} = T_{s} = T_{p} = 1 - R_{0} = \frac{4n_{1}n_{2}}{(n_{2} + n_{1})^{2}}$$

#### Wavelength $\lambda$



For **I** and **v** perpendicular to the surface (i.e.  $\alpha = 0$ ):

$$\mathsf{F}(\lambda,\mathbf{0}) = \left(\frac{\mathbf{n}_{\lambda} - \mathbf{1}}{\mathbf{n}_{\lambda} + \mathbf{1}}\right)^{2} \quad \mathbf{a} \quad \mathbf{n}_{\lambda} = \frac{\mathbf{1} + \sqrt{\mathsf{F}(\lambda,\mathbf{0})}}{\mathbf{1} - \sqrt{\mathsf{F}(\lambda,\mathbf{0})}}$$

quantities F<sub>λ</sub>(0) were measured in labs for many real materials (both conductors and insulators)
 – so we know the n<sub>λ</sub> indices

specular reflection depends on  $\lambda$  (except for  $\alpha = \pi/2$ )



#### **Reflectance – dielectric material**



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#### Reflectance - metal



### **Microfacet theory**



Beckmann, Spizzichino (63), Torrance, Sparrow (67)





## Perfect reflection for half-angle

Only ideal **half-angle microfacets** can contribute !



### Shadowing and masking





#### Multiple bounces are lost







# Microfacet specular BRDF

$$R_{\lambda}(h) = \frac{F_{\lambda}(\alpha)}{4} \cdot \frac{D(h) \cdot G(l, v, h)}{(n \cdot l)(n \cdot v)}$$

- $R_{\lambda}(h)$  ... specular reflectance for wavelength  $\lambda$
- *F<sub>λ</sub>(α)* ... Fresnel ideal reflectance for wavelength λ and incident angle α
- *D(h)* ... microfacet PDF ("how many microfacets" have *h* as a normal vector)
- <u>*G(l,v,h)*</u> ... geometric factor (shadowing & masking)

#### Fresnel term F



Fresnel term for unpolarized light

$$\begin{split} F(\lambda,\beta) &= \frac{1}{2} \cdot \frac{\left(g-c\right)^2}{\left(g+c\right)^2} \begin{cases} 1 + \frac{\left[c\left(g+c\right)-1\right]^2}{\left[c\left(g-c\right)-1\right]^2} \end{cases} \\ \text{for} \quad c = \cos\beta = \left(V \cdot H\right), \\ g^2 &= n_\lambda^2 + c^2 - 1 \end{split}$$

 $\mathbf{n}_{\lambda}$  ... index of refraction for wavelength  $\lambda$ 

• for conductors 
$$\mathbf{n}_{\lambda}' = \mathbf{n}_{\lambda} - \mathbf{i} \kappa_{\lambda}$$
 ( $\kappa_{\lambda}$  ... absorbtion coeff.)



#### Fresnel – base specular color

| Metal     | F(0) [linear]       | F(0) [sRGB]   |  |
|-----------|---------------------|---------------|--|
| Titanium  | 0.542, 0.497, 0.449 | 194, 187, 179 |  |
| Chromium  | 0.549, 0.556, 0.554 | 196, 197, 196 |  |
| Iron      | 0.562, 0.565, 0.578 | 198, 198, 200 |  |
| Nickel    | 0.660, 0.609, 0.526 | 212, 205, 192 |  |
| Platinum  | 0.673, 0.637, 0.585 | 214, 209, 201 |  |
| Copper    | 0.955, 0.638, 0.538 | 250, 209, 194 |  |
| Palladium | 0.733, 0.697, 0.652 | 222, 217, 211 |  |
| Zinc      | 0.664, 0.824, 0.850 | 213, 234, 237 |  |
| Gold      | 1.022, 0.782, 0.344 | 255, 229, 158 |  |
| Aluminum  | 0.913, 0.922, 0.924 | 245, 246, 246 |  |
| Silver    | 0.972, 0.960, 0.915 | 252, 250, 245 |  |



Fresnel term for other angles, based on  $F_{\lambda}(0) = c$ 

$$F_{schlick}(c, l, h) = c + (1 - c) (1 - (l \cdot h))^{5}$$



- let's assume we have a base material color F<sub>λ</sub>(0) and an angle-function for some (standard) λ<sub>0</sub>
  - set of wavelengths can be limited (3÷6 components)

$$F_{\lambda}(\alpha) \approx F_{\lambda}(0) + (1 - F_{\lambda}(0)) \frac{max(0, F_{\lambda_0}(\alpha) - F_{\lambda_0}(0))}{1 - F_{\lambda_0}(0)}$$



Fast and simple formula – Gaussian distribution:

$$D(h,m) = \chi(n \cdot h) (n \cdot h) \cdot e^{-\left(\frac{\delta}{m}\right)^2}$$

- $\chi(a) = a > 0 ? 1 : 0$
- $\cos \delta = \mathbf{n} \cdot \mathbf{h}$
- *m* ... "surface roughness" (standard deviation of the surface slope)
  - **< 0.1** ... very smooth
  - > 0.8 ... rough (almost diffuse)

#### Beckmann's distribution (~normalised)

$$D_{be}(h,m) = \frac{\chi(n\cdot h)}{\pi m^2 (n\cdot h)^4} e^{-\left(\frac{\tan\delta}{m}\right)^2}$$
$$= \frac{\chi(n\cdot h)}{\pi m^2 (n\cdot h)^4} e^{\frac{(n\cdot h)^2 - 1}{m^2 (n\cdot h)^4}}$$



### Blinn-Phong (normalised)

$$\underline{D_{bp}(h,m)} = \chi(n \cdot h) \ \frac{m+2}{2\pi} \ (n \cdot h)^m$$



#### Trowbridge & Reitz

$$\frac{D_{tr}(h,m)}{\pi \left( (n \cdot h)^2 (m^2 - 1) + 1 \right)^2}$$

#### **m** can be greater than 1



#### GGX (Walter et al. 2007)

$$\underline{D_{GGX}(h,m)} = \frac{\chi(n\cdot h) m^2}{\pi (n\cdot h)^4 (m^2 + \tan^2 \delta)^2}$$

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#### Isotropic Ward (1992)



$$\underline{D_{wiso}(h,m)} = \frac{\chi(n \cdot h)}{\pi m^2} e^{-\frac{\tan^2 \delta}{m^2}}$$

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### Anisotropic Ward (1992)

$$D_w(h, m_x, m_y) = \frac{\chi(n \cdot h)}{\pi m_x m_y} e^{-\tan^2 \delta \left(\frac{\cos^2 \phi_h}{m_x^2} + \frac{\sin^2 \phi_h}{m_y^2}\right)}$$

•  $\phi_h$  ... azimuth angle of the half-vector

#### Ашихмин-Shirley anisotropic (2000)

$$D_{as}(h, e_x, e_y) = \sqrt{(e_x + 1)(e_y + 1)} (h \cdot n)^{e_x \cos^2 \phi_h + e_y \sin^2 \phi_h}$$





(с) Ашихмин, 2000

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Idea of blending several materials together makes sense:  $m_1 \dots m_k$ 

$$\mathbf{D}(\alpha) = \sum_{i=1}^{k} \mathbf{w}_{i} \cdot \mathbf{D}(\mathbf{m}_{i}, \alpha)$$

• W<sub>i</sub> ... weight coefficients

 $\Sigma \mathbf{w}_{i} = \mathbf{1}$ 

#### Geometric term G (Cook-Torrance)



Cook and Torrance assumed infinitely long **"V"-shaped grooves** (not exactly true)

#### optimized: Kelemen, more accurate: Smith

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### G alternative (GGX)



$$\frac{G_{GGX}(l, v, h)}{(l, v, h)} = \chi\left(\frac{v \cdot h}{v \cdot n}\right) \frac{2}{1 + \sqrt{1 + m^2} \tan^2 \theta_v}$$

**m** ... roughness from the GGX distribution

#### Cheap G (Kelemen-Szirmay-Kalos)

$$\frac{G_{KSK}(l,v,h)}{(n\cdot v)} \approx \frac{1}{(l\cdot h)^2}$$

# **Blinn's contribution**



- Blinn-Phong model (here  $\beta = \angle v, r$ )
  - light source and viewer in infinity:
  - $\cos^{h}\beta \approx \cos^{4h}\beta/2$  $(R_{i} \cdot V)^{h} \approx (H_{i} \cdot N)^{4h}$





- **Christophe Schlick** (1994) was experimenting with approximate substitution in Fresnel term
- fraction instead of power function  $S^h \approx S / (h - hS + S)$ 
  - slightly less sharp highlight compared to Blinn-Phong
- Fresnel term substitute (32× faster, error <1%)  $R_{schlick}(c, l, n) = c + (1 - c) (1 - (l \cdot n))^{5}$



#### Generalized cosine lobe model

- derived using Householder matrix (3×3)
- 1. classical specular term (Phong) ..

$$f_r(l,v) = \rho_s C_s \cos^h \beta$$

2. .. rewritten using Householder matrix notation

$$f_r(l, v) = \rho_s C_s (r \cdot v)^h$$
  
=  $\rho_s C_s [l^T (2nn^T - I) v]^h$ 



# General plausible cosine lobe

- Householder matrix  $M(3 \times 3)$ 
  - for reciprocity it must be symmetrical

$$f_r(l,v) = \rho_s \left[ l^T M v \right]^h$$

- SVD decomposition of matrix **M**:  $f_r(l, v) = \rho_s \left[ l^T Q^T D Q v \right]^h$
- **Q** ... coordinate transform, **D** ... diagonal matrix

$$f_{r}(l,v) = \rho_{s} \left[ C_{b}l_{b}v_{b} + C_{t}l_{t}v_{t} + C_{n}l_{n}v_{n} \right]^{h}$$

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h

### **Cosine lobe options**



- Phong lobe:  $-C_b = -C_t = C_n = \sqrt{C_s}$
- general isotropic reflection:  $C_b = C_t$
- anisotropy:  $C_b \neq C_t$
- isotropic diffuse term:  $C_b = C_t = 0, C_s = (h+2)/2\pi$
- off-specular reflection:  $C_n < -C_b = -C_t$
- retro-reflections:  $C_b, C_t, C_n > 0$

### **Compound model**



Superposition of several lobes

each one is defined by: C<sub>b,i</sub>, C<sub>t,i</sub>, C<sub>n,i</sub>, h<sub>i</sub>

$$f_{r}(l,v) = \sum_{i} \left[ C_{b,i} l_{b} v_{b} + C_{t,i} l_{t} v_{t} + C_{n,i} l_{n} v_{n} \right]^{h_{i}}$$





#### Lambert law is not perfect..

- pure "cosine" surface is not as common in the nature
- rough, grainy surfaces (sandpaper, sand, etc.)
- full moon contours should be darker but actually they are not !
- "back-scattering" effect, reflecting (passive) taillights





### Oren-Nayar model



#### based on microfacet idea

- diffuse reflection on microfacets
- simplified formulas only most important ones

$$E_{d} = \frac{\rho}{\pi} \cdot E_{0} \cdot \cos(\theta_{i}) \cdot (A + B \cdot max(0, \cos(\phi_{o} - \phi_{i})) \cdot \sin(\alpha) \cdot \tan(\beta))$$

 $\begin{array}{ll} \theta_{i} & \text{incoming angle } (\angle l_{i}, n) \\ \theta_{o} & \text{outgoing angle } (\angle v, n) \\ \Phi_{i} & \text{incoming azimuth of } \omega_{i} \\ \Phi_{o} & \text{outgoing azimuth of } \omega_{o} \\ \alpha & \max(\theta_{i}, \theta_{o}) \\ \beta & \min(\theta_{i}, \theta_{o}) \end{array}$ 





 $E_{d} = (C_{L} \circ C_{D}) \cdot \cos(\theta_{i}) \cdot (A + B \cdot max(0, \cos(\phi_{o} - \phi_{i}))) \cdot \sin(\alpha) \cdot \tan(\beta))$ 

$$A = 1 - 0.5 \cdot \frac{\sigma^2}{\sigma^2 + 0.33}$$

(value in denominator – up to 0.57)

$$B = 0.45 \cdot \frac{\sigma^2}{\sigma^2 + 0.09}$$

- **σ roughness**: mean value of h (see Cook-Torrance)
- C<sub>L</sub> light source color
- C<sub>D</sub> material color

#### **Oren-Nayar - samples**





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